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**Lower between-limb asymmetry during running on**

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**treadmill compared to overground**

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**in subjects with laterally pronounced knee osteoarthritis**

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## 25 **ABSTRACT**

26 Subjects with knee osteoarthritis (KOA) show gait asymmetries evidenced by lower knee  
27 flexion and shorter contact times for the affected leg. Interestingly, running on a treadmill  
28 compared to running overground is also associated with lower knee flexion and shorter contact  
29 times. Thus, it is of particular interest how gait patterns are influenced by the type of ground in  
30 subjects with KOA. The aim of the current study was therefore to measure the overground  
31 asymmetry of kinematic parameters in KOA subjects while running and to investigate whether  
32 this asymmetry is altered on a treadmill.

33 Nine patients diagnosed with KOA underwent overground and treadmill running with 3D-  
34 motion analysis. The symmetry analysis was performed using Symmetry Angles for five  
35 selected gait parameters: contact and step time, heel-toe delay, maximal knee flexion during  
36 stance and vertical speed variance. For all parameters, the values were significantly lower for  
37 the affected compared to the non-affected leg ( $p \leq 0.023$ ). Post-hoc analyses revealed significant  
38 differences between legs only overground and not on the treadmill. The asymmetry was lower  
39 on the treadmill, as indicated by significant Symmetry Angle reductions for contact time  
40 ( $p=0.033$ ), knee flexion ( $p=0.001$ ) and vertical speed variance ( $p=0.002$ ). The symmetry  
41 increase on the treadmill was mainly due to changes of the non-affected leg towards the affected  
42 leg values leading to smaller steps and less impact load in general. The present results suggest  
43 therefore that a) an assessment of symmetry may differ depending on the ground type (treadmill  
44 versus overground) and b) treadmill running may be more suitable for patients with KOA  
45 related gait asymmetries.

## 46 **1. INTRODUCTION**

47 There is good evidence about altered gait kinematics in subjects suffering from chronic knee  
48 osteoarthritis (KOA) when tested during walking. For instance, greater stride duration [1-3] and  
49 lower gait velocity [3, 4], knee flexion [2, 3, 5], peak knee flexion moments, peak hip adduction  
50 moments and peak hip extension moments were found during walking [6]. As these changes  
51 are more pronounced in the injured leg, they have been shown to induce inter-limb asymmetries  
52 for KOA subjects during walking [7].

53 For running, however, there is, to our knowledge, currently no evidence about the influence of  
54 KOA on between-limb symmetry. So far, it has been demonstrated that participants with a non  
55 KOA knee injury display lower mid-stance knee flexion [8, 9], larger pelvis tilt and more hip  
56 internal rotation than healthy controls while running [10]. Leg-injured runners also showed  
57 larger asymmetries in contact time than healthy controls [11]. Based on these examples, we  
58 speculate that subjects with a chronic KOA also display altered gait parameters resulting in  
59 asymmetries during running. To verify this assumption, the first goal of this study was to assess  
60 running patterns of physically active participants with KOA. During running, we expected  
61 lower knee flexion and shorter contact times for the affected leg as already observed for walking  
62 [12].

63 Interestingly, running on a treadmill (TM) compared to running overground (OG) is also  
64 associated with lower knee flexion [13] as well as shorter contact and step times [14, 15]. Thus,  
65 it is of particular interest how gait patterns are influenced by ground types in subjects with  
66 KOA. So far, no study compared the running gait asymmetry between OG and TM locomotion.  
67 This might be problematic, as to our knowledge, all previous studies about leg injury patients  
68 have investigated gait and running patterns either exclusively on TM [1, 9, 11] or exclusively  
69 OG [2, 7, 10] without ensuring the comparability of the assessment of asymmetry between  
70 both ground cases. This may surprise, as there is accumulating evidence that locomotion on the

71 TM and OG differs. For instance, several studies in stroke patients have demonstrated increased  
72 symmetry during walking on the TM compared to walking OG [16, 17]. In addition, running  
73 on a TM displayed more regular stride timing dynamics than running OG [18]. Furthermore,  
74 based on differences in muscular activity between OG and TM, Oliveira et al. [19] assumed  
75 higher demands for load absorption at initial contact for OG compared to TM-running.  
76 Moreover, a flatter foot-landing position lowering the heel-toe delay [20, 21], a reduction in  
77 step length [22], step time, contact time [23], vertical speed variance [14, 23] and maximal knee  
78 flexion during the stance phase [13] were found when subjects switched from OG to TM. As  
79 these adaptations on the TM are independent from gait-alterations due to knee injury, but  
80 nevertheless represent some similarities with adaptations observed OG for the injured leg of  
81 KOA patients, the second and main goal of the current study was to clarify whether TM  
82 locomotion alters the asymmetry-pattern of patients with KOA.  
83 For this purpose, we assessed OG and TM running characteristics of KOA patients with a  
84 special focus on gait symmetry. Kinematic gait parameters were analysed for steps performed  
85 with the affected leg (AL) and the non-affected leg (NL) on TM and OG. The symmetry of  
86 these parameters was expressed by using the so-called Symmetry Angle (SA) [24]. Based on  
87 the literature mentioned above [2, 6, 13], we hypothesized a reduction of the running-  
88 asymmetry on the TM compared to OG.

89

## 90 **2. METHODS**

91 Data for this study were obtained in the same experiment as those published previously in  
92 Schween et al. [25]. We here describe the methods to the extent they are relevant for the current  
93 analysis. The experiment was conducted in accordance with the Declaration of Helsinki and  
94 approved by the ethics committee of the University of Freiburg, Germany (107/12). Before  
95 testing, all participants gave written, informed consent.

## 97 **2.1 Subjects and procedure**

98 Inclusion criterion to the experiment was a medically diagnosed KOA. All the investigated  
99 subjects had a unilateral injury. The KOA injured leg was called “affected leg” AL and the  
100 other one “non-affected leg” (NL). Subjects’s Kellgren-Lawrence grades were between 2 and  
101 3 (mean  $2.8 \pm 0.4$ ). Subjects with neurological disorders, prosthetic implants and any condition  
102 contraindicating the physiological demands of the experiment were excluded. Out of 19  
103 participants that practiced a sport activity at least twice per week, nine were selected for this  
104 analysis, based on the criteria being clear heel runners (6 women and 3 men; mean  $\pm$  standard  
105 deviation:  $50 \pm 9$  years; mass:  $64.6 \pm 9.6$  kg; body size:  $170.1 \pm 9.5$  cm). Seven subjects were  
106 excluded as they did not show a running pattern (some steps showed no flight phase), while  
107 three subjects were not considered as they displayed a forefoot running strategy.

108 Prior to the experiment, the subjects walked for about 5 minutes before running OG for 1 minute  
109 at their natural speed. During the last part of this warm-up process, the natural running speed  
110 was determined with light barriers for each subject. In the actual experiment, subjects were  
111 tested at this self-selected running speed for both OG and TM conditions. The order of ground  
112 types (TM or OG) was randomized to level out fatiguing effects or any other systematic bias.

113 At least ten trials of 10 m corresponding to about ten steps (five on both legs) were captured  
114 OG at target speed  $\pm 0.05$  m/s. This was done by immediately assessing speed with light barriers  
115 and repeating trials outside these limits. In this case, participants were informed in which  
116 direction they had to adjust their speed. The ground forces were measured for both legs on  
117 separate force plates for each trial. On the TM, subjects ran a single bout of about 3 minutes  
118 with the TM speed set to their mean speed as determined during warm-up. After one minute  
119 familiarization, 5 trials of 20 seconds (about 50 steps) were captured.

120 With the above-described procedure, about 100 OG and 200 TM steps were captured and  
121 analysed for each subject. Each step, and by that way both legs, were analysed in each trial.  
122 This procedure reduces any effects that fatigue might have had on the between-leg comparison,  
123 since fatigue would be expected to affect both legs. Furthermore, the current analysis consists  
124 of the measurement of specific parameters (presented in the “data analysis” section) on the base  
125 of all trials. The final parameters correspond to the arithmetic average of the measurements  
126 from all trials and that for OG and TM, and for AL and NL.  
127 Standardized shoes (Spezial, Adidas®, Herzogenaurach, Germany) with low cushioning and  
128 no custom insoles were worn throughout the experiment to prevent potential footwear-related  
129 effects.

130

## 131 **2.2 Equipment and data collection**

132 The kinematics of the lower extremity were assessed using a 3D-motion analysis system (Vicon  
133 V-MX, VICON Motion Systems Ltd., Oxford, UK) at a sampling frequency of 200Hz by  
134 placing reflecting markers on the pelvis, thigh, lateral and medial epicondyle of the knee, both  
135 malleoli, shanks and feet (in line with [25]). The VICON system has a marker position precision  
136 of about 2mm [26] and a time precision of about 2.5 ms due to its sampling rate. Overground,  
137 we measured the average running speed using light barriers (Timer S3, ALGE, Maienfeld,  
138 Switzerland; with a precision below 0.001 m/s) and the ground reaction force with a force plate  
139 (BP600900-2000, Advanced Mechanical Technology Inc., Watertown, MA, USA) at a sample  
140 rate of 2000Hz. The used treadmill (quasar 5.0, h/p/cosmos sports and medical GmbH,  
141 Nussdorf-Traunstein, Germany) was new and was, prior to the experiment, directly installed by  
142 the equipment provider. No specific speed and slope calibration [27] was therefore required.  
143 The slope was set at 0% by a motorized adjustment and the naturally selected speed was  
144 programmed with a precision of 0.1m/s. Kinematic data was synchronized to ground reaction

145 forces in the OG condition and both signals were low-pass filtered at 15Hz (4<sup>th</sup> order  
146 Butterworth, bidirectional, in line with Schween et al. [25].

147

## 148 **2.3 Data analysis**

149 We selected those kinematic parameters for our analysis that had previously been shown to  
150 differ between KOA-patients and healthy controls [1-5] as well as between OG and TM  
151 locomotion [13, 14]. These were *a) contact time*, *b) step time*, *c) heel-toe-delay*, and *e) vertical*  
152 *speed variance*. Data were analysed with Matlab (The Mathworks, Inc., Natick, Massachusetts,  
153 USA) to determine the kinematic parameters with high reliability as follows [28]: The  
154 arithmetic average of the four pelvis markers placed at the left respective right posterior and  
155 anterior superior iliac spine was used to define the centre of pelvis (CP), which can be  
156 considered as an approximation of the centre of mass [29]. CP velocity and acceleration were  
157 obtained by derivation of the CP position in the sagittal plane.

158 *a) The contact time ( $t_c$ )* was defined as the time between touch-down and take-off, which were  
159 assessed OG by force plate signals. For the TM case, we first measured OG the individual  
160 average delay between touch-down and time of minimal heel elevation for each subject and  
161 each leg. This delay was due to the small skin and marker displacement relative to the  
162 calcaneus. Second, we obtained the time of touch-down on the TM by subtracting this delay  
163 from the minimal heel elevation time. The TM take-off time was determined in a similar way:  
164 the average delay between the time of lowest toe elevation and take-off (determined by the  
165 abrupt nullification of the force plate signal) was measured OG. This delay was added to the  
166 TM time of lowest toe elevation in order to obtain the TM take-off time.

167 *b) The step time ( $t_s$ )* of the AL was defined as the time between the touch-down of AL and the  
168 touch-down of the NL and vice versa.

169 c) Furthermore the *heel-toe delay (HTD)* was defined as the time between touch-down and toe  
170 touch (corresponding to an abrupt cessation of the toe marker vertical velocity).

171 d) The *maximal knee flexion ( $\alpha$ )* during ground contact was determined by analysing the  
172 respective joint angle for each measured time frame and selecting the minimal knees angle  
173 obtained during the stance phase.

174 e) Finally, we determined the *vertical speed variance (VSV)* as the peak-to-peak variation of  
175 the CP vertical velocity during the stance phase (Fig 1). All mentioned parameters were  
176 assessed for both legs (NL/AL) and for both OG and TM cases. Subsequently, the between-leg  
177 differences of each parameter:  $\Delta (X_{NL} - X_{AL})$  were calculated for OG and TM.

178

179 **Fig 1. Running phases with maximal knee flexion and Centre of Pelvis vertical movement**

180 **as a function of time.** The top panel is a schematic representation of a human running in sagittal  
181 plane with contact and flight phases. CP represents the centre of pelvis and  $\alpha$  the maximal knee  
182 flexion during stance for the affected and the non-affected leg (AL, NL). The lower three panels  
183 show the CP height, vertical speed and vertical acceleration measured during an overground  
184 (OG) gait cycle for one KOA patient. The vertical speed variance corresponds to the difference  
185 between minimal and maximal vertical speed during stance (illustrated for both AL and NL).  
186 Note the larger vertical movement and speed variance for NL.

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189 For an assessment of the bilateral symmetry of each kinematic parameter, we used the  
190 Symmetry Angle from Zifchock et al., [11, 24]:

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$$192 \quad SA = \frac{45^\circ - \arctan(X_{AL}/X_{NL})}{90^\circ} \cdot 100 \quad (1)$$

193



194 with  $X_{AL}/X_{NL}$  being the parameter ratio for AL and NL. Note that in equation 1, an SA value  
195 of zero indicates perfect symmetry between the NL and AL. In contrast to the symmetry index  
196 [30], the SA is not prone to problems of normalization and does not require an adequate  
197 reference value [24].

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## 199 **2.4 Statistics**

200 The parameters:  $t_c$ ,  $t_s$ , HTD,  $\alpha$  and VSV were statistically tested with separate two-way repeated  
201 measure analysis of variance (SPSS 19, Inc. Chicago, IL, USA), taking into account the LEG  
202 (NL/AL) and GROUND (OG/TM) factors. Subsequently, post-hoc tests were applied by using  
203 Bonferroni-corrected paired Student's  $t$ -tests to specify differences between NL and AL for  
204 each ground type and between OG and TM for each leg.

205 Symmetry Angles for each independent parameter were compared between OG and TM using  
206 paired Student's  $t$ -tests. The two-sided significance level was set at 5% and data are reported  
207 as means  $\pm$  standard deviations in the text.

208

## 209 **3. RESULTS**

210 The average running velocity, took identical values of  $2.4 \pm 0.3$  m/s for both OG and TM.  
211 Results of the five kinematic parameters with their NL/AL side dependency are shown in Fig 2  
212 for both ground types. In paragraph 3.1, the differences between NL and AL, and between OG  
213 and TM are presented together with the interaction between LEG and GROUND factors. The  
214 Symmetry Angles of each kinematic parameter are described in paragraph 3.2.

215

216 **Fig 2. Kinematic parameters side dependency for OG and TM ground.** A) Overall results  
217 of the kinematic parameters for overground (OG) and treadmill (TM) running. NL refers to the

218 non-affected leg and AL to the affected leg. Boxplots show the results over all subjects. For  
219 each boxplot, the middle line represents the median value, the lower and upper limits represent  
220 the interquartile range and the error bars indicate the range and the plus signs denote outliers.  
221 Stars (\*, \*\*, \*\*\*) indicate significant differences ( $p < 0.05$ ,  $p < 0.01$ ,  $p < 0.001$ ) between NL and  
222 AL. Note that OG the differences between the NL and the AL were larger for all kinematic  
223 parameters compared to when running on the TM. B) Difference between the NL and AL value  
224 for all parameters. With dotted lines representing full symmetry, a symmetry increase is  
225 observed for all parameters.

226

### 227 **3.1 Kinematic parameters**

228 We found significant main effects for LEG, with AL displaying lower values than NL for all  
229 parameters as illustrated in Fig 2:  $t_c$  (-1.6%,  $F_{1,8} = 45.4$ ,  $p < 0.0002$ ),  $t_s$  (-2.9%,  $F_{1,8} = 7.84$ ,  
230  $p = 0.023$ ), HTD (-12.2%,  $F_{1,8} = 9.16$ ,  $p = 0.016$ ),  $\alpha$  (-7.5%,  $F_{1,8} = 10.9$ ,  $p = 0.011$ ) and VSV  
231 (-8.3%,  $F_{1,8} = 9.95$ ,  $p = 0.013$ ). On the other hand, the GROUND condition showed a significant  
232 reduction on TM only for the step time and the maximal knee flexion:  $t_s$  (-4.2%,  $F_{1,8} = 49.3$ ,  
233  $p < 0.0001$ ) and  $\alpha$  (-4.5%,  $F_{1,8} = 6.8$ ,  $p = 0.03$ ) while a trend towards lower TM values was  
234 observed for HTD (-19.3%,  $F_{1,8} = 4.72$ ,  $p = 0.061$ ).

235 The contact time, maximal knee flexion and vertical speed variance revealed significant  
236 interactions between LEG and GROUND factors:  $t_c$  ( $F_{1,8} = 5.67$ ,  $p = 0.044$ ),  $\alpha$  ( $F_{1,8} = 25.4$ ;  
237  $p < 0.001$ ) and VSV ( $F_{1,8} = 19.7$ ,  $p = 0.002$ ).

238 Interestingly, the post-hoc analyses of all parameters (except the step time) revealed significant  
239 reduction for the AL only OG and not on TM (Fig 2):  $t_c$  (OG - 2.7%,  $t_8 = 5.94$ ,  $p = 0.0014$ ; TM:  
240 - 0.5%,  $t_8 = 0.88$ ,  $p > 0.9$ ), HTD (OG: -13.2%,  $t_8 = 3.83$ ,  $p = 0.02$ ; TM: -10.8%,  $t_8 = 2.04$ ,  $p =$

241 0.3),  $\alpha$  (OG: -8.8%,  $t_8 = 3.91$ ,  $p = 0.018$ ; TM: -6.1%,  $t_8 = 2.66$ ,  $p = 0.12$ ) and VSV (OG: -9.4%,  
242  $t_8 = 5.59$ ,  $p=0.028$ ; TM: -7.1%,  $t_8 = 2.68$ ,  $p=0.11$ ).

243

### 244 **Between leg differences of kinematic parameters**

245 All parameters showed a reduction of their between leg difference:  $\Delta = (X_{NL} - X_{AL})$  when switching  
246 from OG to TM (see Fig 2b) with significant reductions observed for  $t_c$ ,  $\alpha$  and VSV. The  
247 between leg difference of  $t_c$  almost disappeared on the TM while for the other parameters,  $\Delta$   
248 was reduced by roughly 30%.

249

### 250 **3.2 Symmetry analysis**

251 We calculated the Symmetry Angle for all kinematic parameters using equation (1) for both  
252 OG and TM, and show the results in Fig 3. Symmetry was significantly increased when subjects  
253 switched from OG to TM indicated by a reduced SA for contact time (-80%; OG:  $0.86 \pm 0.38$ ;  
254 TM:  $0.17 \pm 0.52$ ;  $t_8 = 2.58$ ,  $p = 0.033$ ), maximal knee flexion (-33%; OG:  $3.0 \pm 2.4$ ; TM:  $2.0 \pm$   
255  $2.3$ ;  $t_8 = 4.96$ ,  $p = 0.001$ ) and vertical speed variance (-28%; OG:  $3.3 \pm 3.1$ ; TM:  $2.4 \pm 2.8$ ;  $t_8 =$   
256  $4.38$ ,  $p = 0.002$ ). The Symmetry Angles for step time (OG:  $1.0 \pm 1.2$ ; TM:  $0.8 \pm 1.1$ ;  $t_8 = 0.52$ ,  
257  $p = 0.62$ ) and heel-toe delay (OG:  $4.8 \pm 3.3$ ; TM:  $3.1 \pm 4.6$ ;  $t_8 = 0.97$ ,  $p = 0.36$ ) displayed no  
258 differences between ground conditions. These results thus corroborate those based on between-  
259 leg differences.

260

### 261 **Fig 3. Overall results of the Symmetry Angle for overground (OG) and treadmill (TM).**

262 Boxplots show the results over all subjects with dotted lines corresponding to lines of full  
263 symmetry and stars indicating significant differences. We observe a Symmetry Angle decrease  
264 on TM compared to OG for all parameters, revealing a general symmetry increase on the TM.

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266

## 267 **4. DISCUSSION**

268 The present study demonstrated significant differences between the ALs and NLs when  
269 measured OG. However, these asymmetries were effectively reduced when running was  
270 performed on TM.

271

### 272 **Differences between affected and non-affected leg overground**

273 Previous studies compared the affected legs of runners with various knee injuries to the  
274 unaffected legs of healthy controls [8, 9, 31, 32]. In that respect, knee-injured subjects displayed  
275 lower knee flexion than non-injured subjects [8, 9]. These differences between injured and  
276 healthy subjects are in line with the differences between the AL and the NL observed OG in  
277 the current study: a significantly smaller knee flexion occurred in the AL than the NL.  
278 Furthermore, all other parameters except step time, thus, contact time, heel-toe delay and  
279 vertical speed variance, also displayed significant differences between AL and NL when  
280 measured OG (see Fig 2). Interestingly, large differences between the AL and the NL of about  
281 10% were found OG for maximal knee flexion, vertical speed variance and heel-toe delay. All  
282 these parameters were associated with high (near maximal) vertical movement dynamics, i.e.,  
283 ground reaction forces. Indeed we find in Fig 1 as previously observed [33] a nearly maximal  
284 ground reaction force ( $F = m \cdot a$ , assuming that the lower panel Pelvis acceleration “a” is a good  
285 approximation of the centre of mass acceleration) at the time of maximal knee flexion (dotted  
286 lines). In contrast, step time and contact time, which are not directly linked to the peak of the  
287 vertical movement dynamics, displayed bilateral differences of only about 3% when measured  
288 OG (Fig 2a). Thus, larger asymmetries occurred during movement phases incorporating high  
289 (almost maximal) loading of the affected structure, i.e. the knee, in the vertical direction. Lower  
290 knee flexion in leg-injured subjects has often been interpreted as a protective mechanism

291 against knee pain [8, 34, 35]. It seems reasonable that, especially during vertical movements of  
292 the body, high forces acting on the knee may be associated with the occurrence of pain in the  
293 AL, causing avoidance behaviour that leads to bilateral asymmetries. Similarly, the heel-toe  
294 delay proved to be very sensitive to knee injury (asymmetry of 13%). Although there is not  
295 much force at the beginning of the heel touch, considerable force is built up during the transition  
296 to the toe touch (see the vertical acceleration in Fig 1). It is noteworthy that the force level at  
297 the time of toe touch is considerably lower in the AL compared to the NL (Fig 1) as the delay  
298 between heel touch and toe touch is shorter. At the same time, this shorter heel-toe delay in the  
299 AL presupposes a flatter foot-landing position. Previous research has assumed that flatter foot-  
300 landing positions might be perceived as more stable for runners [20]. Consequently, patients  
301 with knee problems may prefer a more stable landing position for their AL. Alternatively it may  
302 be speculated that although the ground reaction forces are not high at the time of the heel-touch,  
303 it is known that pronounced rear foot strike patterns increase external knee flexion moment  
304 [36]. Therefore, knee patients may prefer a fast transition to the toe touch in order to reduce  
305 knee flexion moment.

306

### 307 **Treadmill-induced changes in running symmetry**

308 The reduction of the AL-NL asymmetry on the treadmill is highlighted by considering (a) the  
309 bilateral percentage differences (Fig 2b) and (b) the Symmetry Angle (Fig 3) for both ground  
310 conditions. As the results of these two analyses are very similar, we concentrate now on the  
311 SA. The KOA subjects of the current study displayed larger SAs OG for the knee flexion,  
312 vertical speed variance and heel-toe delay ( $SA > 3$ ) compared to the step and contact time (SA  
313 close to 1). Running on the treadmill induced significant reductions of SA between 28% and  
314 80% for the contact time, knee flexion and the vertical speed variance (Fig 3). However,  
315 changes in the heel-toe delay and the step time were not significant (see Fig 3). For the heel-

316 toe delay, large variations within and across subjects were observed making it difficult to find  
317 systematic adaptations (Fig 2). For the step time, the reason for the non-significance could be  
318 related to the fact that the step time is not under the permanent influence of high vertical forces.  
319 It therefore seems that symmetry was mainly altered on the TM during times of large ground  
320 reaction forces, which may seem counterintuitive at first glance. It is therefore important to  
321 analyse in detail how changes of the AL and the NL contributed to the enhanced symmetry.  
322 Interestingly, the enhanced symmetry on the TM mainly relied on adaptations of the NL. This  
323 was particularly visible for the contact time where the reductions on the TM were three and a  
324 half times larger for the NL than for the AL resulting in a drop of the SA of 80%. Changes in  
325 the NL also played the essential role for the vertical speed variance, where a trend towards  
326 reduction on the TM was only observed for the NL while the AL showed identical average  
327 values in both ground conditions (Fig 2). Thus, the adaptations that occur naturally on the TM  
328 such as flatter foot landing [20], reduced stance time, knee flexion and peak ground reaction  
329 force [14], help to restore symmetry as they go into the same direction for the healthy leg as the  
330 adaptations due to knee injury. In contrast, the AL seems to display a ceiling effect as the values  
331 hardly change when switching from OG to the TM.

332

333 The current results, showing large differences regarding the symmetry between OG and TM  
334 running, indicate that the type of ground greatly influences the sensitivity of detecting gait  
335 asymmetries. While all parameters except step time were significantly asymmetrical OG, none  
336 of these parameters was significantly different between AL and NL on the TM (see Fig 2).  
337 These observations corroborate the significant decrease of the SA on TM for the contact time,  
338 maximal knee flexion and vertical speed variance parameters. Thus, it seems that TM running  
339 masks KOA-induced gait asymmetries. This underlines the importance of taking into account  
340 ground conditions in order to make valid comparisons between studies with different ground

341 types and when evaluating patients with KOA. Finally, with respect to rehabilitation and  
342 decreased asymmetry, the current study indicates that TM-training may be preferable over OG-  
343 training for KOA patients as the former restored gait symmetry.

344 The study had however some limitations: first of all, we only studied nine subjects which can  
345 reduce the statistical significance of the analysis. However, all subjects displayed the same  
346 behaviour between OG and TM for SA of four kinematic parameters. Secondly, only subjects  
347 with a light KOA injury could participate to the experiment, because they had to be able to run  
348 OG and on TM. A third limitation comes from the kinematic parameters that have been defined  
349 in the OG case. The ground reaction force signals were compared with the VICON foot markers  
350 behaviour to determine touch down and take-off times. If the reliability of the method could be  
351 verified for OG trials, this was not the case for the TM measurements. A treadmill allowing the  
352 measurement of the ground reaction force [37] would permit to fully validate the definition  
353 method of the kinematic parameters in the TM condition.

354

## 355 **5. CONCLUSION**

356 Our study showed that running gait symmetry in KOA patients was increased on a TM  
357 compared to OG. This was indicated by significant improvements in Symmetry Angle when  
358 switching from OG to the TM. Interestingly, the symmetry increase was mainly due to  
359 adaptations of the non-affected leg. The increased symmetry on TM for the investigated  
360 parameters stresses the importance of taking into account the ground type when analysing gait  
361 symmetry. In addition, the current results suggest that for the recovery of gait symmetry in  
362 KOA-patients, interventions on TM may be preferable.

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